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"Water Related Disaster Solutions"

SHERATON MUSTIKA YOGYAKARTA, INDONESIA SEPTEMBER 6th - 8th, 2013





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PREFACE



The International Seminar with special focus on "Water Related Disaster Solutions" was implemented successfully from 6th to 8th September 2013 in Yogyakarta attended by experts and professionals from many countries including Indonesian as the host.

The discussions of the Seminar had covered the entire aspects of the water related disaster solutions including its risk management, the innovation in disaster mitigation and adaptation, as well capacity building and community participation aspects, involving highly notified professionals with numerous technical models, state of the arts as well as scientific and empirical deliberations.

The overall presentations, discussions and debates during the Seminar concluded that the outputs will undoubtedly contribute to remarkable concepts, strategies, lessons learned, and sharing of experiences on the water related disaster solutions, particularly on the environmentally sound technologies and sustainable practices on the years to come. Based on this fact, I believe that the proceeding of this Seminar will be valuable document for the implementation of the adaptation and mitigation to the climate change.

I would like to thank the organizing committee, peers and writers, seniors and all members of HATHI for enormous supports to the Seminar. May God bless you all.

Dr. Ir. Moch. Amron, M.Sc., PU-SDA

Chairman of HATHI,

September, 2013

TABLE OF CONTENTS

PRI	EFACE	iii
TA]	BLE OF CONTENTS	v
TA]	BLE OF CONTENTS VOLUME 2	ix
	B THEME 1 k Management in Water-Related Disaster	
1.	Action and Activities for Large Scale Sediment-Related Disasters in the Kii Peninsula, Japan — Takasue Hayashi, Atsushi Okamoto, Naoki Imamori, and Tsuyoshi Nagamachi	1
2.	Sedimentation Effects in Reservoir Toward The Declining Function of Flood Control — Pranoto Samto Atmojo, Kirno, Bertha Silvia Pratiwi	11
3.	Monitoring of Slope Deformation for Early Warning Against Shallow Landslide - Katsuo Sasahara	23
4.	Operation Analysis of Sutami Reservoir Due to the Climate Change in Malang Regency of East Java	33
5.	Sediment Budget, Shoreline Changes, and Groin Performance After Nusa Dua Beach Nourishment Project, Bali, Indonesia — Soni Senjaya Efendi and Dede M. Sulaiman	46
6.	Ratio Between Maximum and Minimum Discharge as an Anticipated Indicator of River Disaster	55
7.	Regional Scale Landslide Susceptibility Zonation in Nepal Himalaya – Ranjan Kumar Dahal and Manita Timilsina	62
8.	Slope Stability Analysis of Landslide Between Km 66+500 and Km 104+420 Along the Mechi Highway, Eastern Nepal	73
9.	Flood Study of Sub-Catchment Buah in Palembang Using Spatial Analyses and Hydraulic Modelling — Rahmadi and Sumi Amariena Hamim	82
10.	Risk Assessment Approach for Climate Change Adaptation in Tanjung Api-Api Port Area Banyuasin Valley, South Sumatera — Achmad Svarifudin, Yunan Hamdani, and Hendri	93

11.	Flood Resiliency Strategy of Kampung Ratmakan, Code Riverside Settlement, Yogyakarta — Rr. Vicky Ariyanti and Andie Arif Wicaksono	115
12.	Contribution of Karian Dam for Flood Protection in Ciujung River Basin Using Two Dimensional Modelling — Yadi Suryadi, Dian Indrawati, Suardi Natasaputra, Ni Luh Putu Adi Ariestuti, Evi Fauziah, Riswanto Rosi, Dian Mahdi Hidayat, and Dian Insani	125
13.	Construction of the Karalloe Multipurpose Dam as Disaster Solution for Raw Water Crisis and Flood in Bontosunggu – Subandi , Hariyono Utomo, Zainal Arifin, and Agus Setiawan	135
14.	The Application of Retention Pond System to Control Flooding in Southern Pontianak City – Jane E. Wuysang and Doddi Yudianto	145
15.	Effective Flood Control through Integrated and Collaborative Operation of Three Dams in Japan	154
16.	Flood Peak Discharge Equation at Surrounding Gembong Watershed, Pasuruan District, East Java, Indonesia – Laksono D. Nugroho, M. Bisri, Lily Montarcih, and Aniek Masrevaniah	166
17.	Water Resources Drought: Hydrological Drought in Developed River Basins — Waluyo Hatmoko, R. Wahyudi Triweko, and Iwan K. Hadihardaja	177
18.	Strategy in Controlling River Bed Degradation in Brantas River Basin – Ni Made Sumiarsih	188
19.	 Development of Emergency Monitoring Device for Natural Dam. Teruyoshi Takahara, Koji Morita, Takao Yamakoshi, Akihito Kaji, Yosuke Ito, Toshiki Yanagimachi, Takeshi Shimizu, and Tadanori Ishizuka 	198
20.	Numerical Simulation of Dam Break using Finite Volume Method: Case Study of Situ Gintung — Bobby Minola Ginting, Bambang Adi Riyanto, and Herli Ginting	206
21.	Application of Rainfall Radar and Runoff Model to Volcanic Mountain Watersheds - Shusuke Miyata, Masaharu Fujita, Takuji Teratani, Hirofumi Tsujimoto, and Takeshi Osaka	218
22.	Numerical Solution of River Flood and Dam Break Problems by Cell Centred Finite Volume Scheme — Dantje K. Natakusumah, M. Syahril Badri Kusuma, Dhemi Harlan, M. Rizky Ramadhan, and Bobby Minola Ginting	224
23.	Drought Analysis Using EDI and SPI Method to Mitigate Drought Disaster in Wonogiri District – Karlina, Joko Sujono, and Rachmad Jayadi	239

24.	Analysis of Reservoir Utilization in Middle Stream Ciliwung as Mitigation and Adaptation of Flood Disaster in Central Jakarta – Rommy Martdianto	250
25.	Predicting the water level of Natural DAM in Ambon, Maluku, Indonesia – Koji Morita, Tadanori Ishizuka, Takao Yamakoshi, Takeshi Shimizu, Akihito Kaji, Reiko Akiyama, Hisaya Sawano, Yosuke Ito, Toshiki Yanagimachi, A. Tommy M. Sitompul, Fajar Wicaksono, William M. Putuhena, Isnan F. Akrom, and Sutiyono	263
26.	Emergency Response Against Water Quality Accident to Secure Safe Water Supply for Capital Area – Satoshi Ojima and Koji Tsuboi	271
	B THEME 2 novation in Disaster Mitigation and Adaptation	
27.	The Role of Sabo Works in The Water-Sediment-Related Disaster Mitigation in Indonesia — Bambang Hargono, Joko Cahyono, and Djoko Legono	283
28.	Sediment Related Disasters in Japan (Experiences and Countermeasures) – Yukihiko Sakatani	291
29.	Routing of Local Inundation as Performed by Polder System in East Jakarta. – Adam Pamudji Rahardjo, Puji Harsanto, and Djoko Legono	301
30.	Model of Mockwyn-UB for Assesing Water Availability Due to The Effect of Climate Change — I Wayan Sutapa, Moh. Bisri, Rispiningtati, and Lily Montarcih	311
31.	The Effectiveness of Coastline Protection Structure at Estuary of Batang Kambang, West Sumatra — Bambang Istijono, Ali Musri, and Rahmad Yuhendra	323
32.	Theoretical Approach of Long Shore Current Reduction Coefficient through Permeable Groin – Hasdinar Umar, Nur Yuwono, Radianta Triatmadja, and Nizam	332
33.	Early Warning System as a Preventive Measure for Landslide Risk Reduction in Kabilash Village, Chitwan District, Nepal	342
34.	The Performance of Perforated Screen Seawall in Dissipating Waves, Minimizing Reflected Wave and Run-Up/Run-Down - Muhammad Arsyad Thaha, A. Ildha Dwipuspita, Willem Minggu, and Haeruddin	355
35.	Hydraulic Intervention Impact on Subsidence and Carbon Emissions of Peatland as a Disaster Mitigation Effort at Sei Ahas - Central Kalimantan – L. Budi Triadi , Aljosja Hooijer, Ronald Vernimmen, and Surya Dharma	365

36.	Consideration in Choosing The Appropriate Flood Control System for Tenggarong River – Doddi Yudianto and Steven Reinaldo Rusli	376
37.	Simple Analytical Solution of Wave Transmision through Submerged Coastal Structure — Chairul Paotonan, Nur Yuwono, Radianta Triatmadja, and Bambang Triatmodjo	389
38.	Innovation of Water-Trap Series Construction and Vetiver Grass in Disaster Mitigation and Adaptation – Susilawati, and Pupun Adi Awi Andi	399
39.	A Method for Prediction of Formation of Landslide Dams Caused by Heavy Rainfall in Kii Peninsula, Japan Hefryan Sukma Kharismalatri, Hitomi Kikuchi, Yoshiharu Ishikawa, Takashi Gomi, Katsushige Shiraki, and Taeko Wakahara	410
40.	The Evaluation of Retention Pond Capacity under a Series of Rainfall Occurence and Land Development — Albert Wicaksono and Doddi Yudianto	419
41.	Rainfall-induced Landslide Hazard Zonation along the Road Side Slopes of Central Nepal – Manita Timilsina and Ranjan Kumar Dahal	428
42.	Influence of Rectangular Lay-out of Underwater Sill to the Flow Patterns and Sediment Transport – Tania Edna Bhakty, Nur Yuwono, Radianta Triatmadja, and Bambang Triatmodjo	439
43.	Integrating the Existing Warning and Evacuation Systems against Debris Flow in Area of Merapi Volcano – Sutikno Hardjosuwarno, Bambang Sukatja, and Dyah Ayu Puspitosari	449
44.	Correlation of Drought and Atmospheric Isotopologues in Indonesia – Samuel J. Sutanto, G. Hoffmann, W. Adidarma, and T. Röckmann	460
45.	Debris Flow and Flash Flood at Putih River after the 2010 Eruption of Mt. Merapi, Indonesia – Yutaka Gonda, Djoko Legono, Bambang Sukatja, and Untung Budi Santosa	471
46.	Simulations of Pyroclastic Flows at Mt. Merapi – Kuniaki Miyamoto , Haruka Matsuyoshi, Djoko Legono, and Masaharu Fujita	481
47.	Numerical Simulation of Tsunami Force on building Using Smoothed Particles Hydrodynamics — Kuswandi, R. Triatmadja, and Istiarto	492

TABLE OF CONTENTS VOLUME 2

PRI	EFACE	iii
TA]	BLE OF CONTENTS VOLUME 1	V
TA]	BLE OF CONTENTS	ix
	B THEME 3 pacity Building for Water Resources Management	
1.	Cascade Weir as a Solution to Prevent Damage of Linamnutu Weir as Caused by Flood Disaster – James Zulfan, Irwan Syafri, and Erman Mawardi	1
2.	Effectiveness and Issues on Portable Seawater Desalination Equipment as Preparedness For Disaster - Kohei Kamata, Mika Deguchi, and Machiko Higa	16
3.	The Effect of Debris on Tsunami Velocity – Siti Nurul Hijah, Kuswandi, Benazir, and Radianta Triatmadja	27
4.	Wetted Perimeter Method for Environmental Flow Assessment of Sekampung River at Argoguruh – E. P. Wahono, D. Legono, Istiarto and B. Yulistiyanto	33
5.	Tsunami Focusing along a Valley of Linearly Varying Width and its Effect on Building — Radianta Triatmadja, and Muhammad Hafiz Aslami	40
6.	Landcover Change and its Effect on Soil Erosion and Economic in Manjuto Watershed of Indonesia — Gusta Gunawan, Dwita Sutjiningsih, and Herr Soeryantono	52
7.	Integrated Investigations for Slip Surface Determination in the Landslide-affected Area of The Blue Nile Gorge, Central Ethiopia – Getnet Mewa and Leta Alemayehu	65
8.	Lessons from The Application of Low Crested Breakwaters as an Alternative Structure for Coastal Protection – D. M. Sulaiman, M.E. Sudjana, Suprapto, R. M. Azhar	77
9.	Priority Strategy using Sensitivity Analysis for Related Policy on Water Disaster — Dian Indrawati, Iwan Kridasantausa, Yadi Suryadi, and Agustin Purwanti	88
10.	Water Quality Monitoring and Data Quality Assurance – Sri Puji Saraswati, Sunjoto, B. Agus Kironoto, Suwarno Hadisusanto, and Eko Sugiharto	99

11.	Japan's Stormwater Management Policy Shift Coresponding to Current Issue				
	 Junichi Yoshitani, Masaki Kawasaki, Yoshito Kikumori, and Shuichi Tsuchiya 				
12.	Flood Disaster and Early Warning System in Thailand – Thada Sukhapunnaphan	118			
13.	Effect of Bed Shear Stress on Static Armour Layer – Cahyono Ikhsan, Adam Pamudji Raharjo, Djoko Legono, and Bambang Agus Kironoto	127			
14.	Hydraulics of Flow through Underground Tunnel to Reduce Flood Disaster Risk of Ciliwung River. — William Putuhena, A. Setiadi, and D. Legono	138			
15.	Disaster Caused by Typhoon Bopha in Southern Mindanao – Takaaki Kusakabe and Oscar Victor Lizardo	146			
16.	Urgent Recovery and Risk Management on Embankment and Lifeline - Case of 2011 Earthquake — Tsuyoshi Tani , Kazuyasu Ishibashi, and Nobuyoshi Akiba	156			
17.	Flood Area Mapping by Using Computed River Overflow – Irfan Kusnadi and Istiarto	168			
18.	A Catastrophic Flash Flood Caused by High Altitude Rockslides in Nepal Himalaya — Daisuke Higaki, Hiroshi Yagi, Hidetomi Oi, Nobuhiro Usuki, and Kosuke Yoshino	179			
19.	Water Allocation Policies In Dodokan River Basin Based On Mros – Galuh Rizqi Novelia, Nadjadji Anwar, and Edijatno	191			
20.	Physical Model to Study the Hydraulic Performance of Bener-Dam Spillway at Bogowonto River – Bambang Yulistiyanto and Djoko Legono	200			
21.	The Impact of Hydrodynamic Flow into River Bed Alternation of Lobawang River, Sitobundo	209			
22.	Rational, Organized, and Successful Emergency Operation against Disaster: Case of the Historic Earthquake in Japan – Satoru Takagi, Kouki Azuma, and Kenji Someya	220			
23.	Development of GIS-based Sediment Runoff Model and Its Application – Masaharu Fujita, Kazuki Yamanoi, and Daizo Tsutsumi	232			

SU	B THEME 4	
Co	mmunity Participation in Disaster Management	
24.	Early Warning for Landslide Hazards Based on Community Participation: Case Study of Padang Pariaman District, West Sumatera, Indonesia – Zahrul Umar, Lili Warti, and Idzurnida Ismael	247
25.	Community Participation in Flood Control Management – Bambang Priyambodo	260
26.	Community Perception on the Implementation of Infiltration Wells in Urban Areas for Reducing Disaster Risk — Widandi Soetopo and Dwi Priyantoro	270
27.	Community Empowerment in Watershed Conservation as Disaster Management in Brantas River Basin, Indonesia – Astria Nugrahany and Erwando Rachmadi	278
28.	Green Open Space on Development of Urban Community-based for Supporting Zero Delta Q Policy	288
29.	IWRM Approach on Water and Disasters: Report in United Nation's Special Session — Tadashige Kawasaki	30
30.	Relevance of Community Led Disaster Response in Aotearoa New Zealand to International Context — Te Kipa Kepa Brian Morgan, Tumanako Ngawhika Fa`aui, and Pia Bennett	314
31.	A study of Community-Based Disaster Preparedness by Making Disaster Prevention Map in Ambon. — Tokunaga Yoshio . Harvono Hansen Sirait, Erfien Kaparang Novivanti	324

THE APPLICATION OF RETENTION POND SYSTEM TO CONTROL FLOODING IN SOUTHERN PONTIANAK CITY

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Abstract

Southern Pontianak is generally situated on lowland area with elevation varies between -0,224 m and +1,959 m. Due to its low elevation, this area is strongly affected by tidal flow. Compared to the highest tide elevation observed by PT. Barunadri Engineering Consultant at +0,213 m, it is obvious that the area is also vulnerable to inundation. Worse situation occurs as there are two channel, Sungai Jawi channel and Sungai Raya Dalam channel, which are frequently flooded during high rainfall intensity. An integrated and sustainable water management is therefore required to mitigate the flooding. Started by identifying the channel capacity to deliver flood flow, the analysis is extended to estimation of series of retention pond to control the flood. The 1-D Duflow model is employed here to simulate the water surface profile along the channels reach and estimate the capacity of ponds. Based on the simulation results, the dimension of two retention ponds required at Sungai Jawi Channel and Sungai Raya Dalam Channel are 700x 700 x 4 m³ and 350 x 350 x 4 m³ respectively. These two retention ponds are designed to control 5 years flood with maximum amount of 1,750,650 m³ and 454,740 m³ under maximum tidal condition.

Keywords: flood control, retention pond, Pontianak City

INTRODUCTION

General Background

Pontianak City is located at the downstream of Kapuas River about 13 kilometers from the estuary of Kapuas River. At the southern side, the land is generally situated on lowland area with elevation varies between -0,224 m and +1,959 m. As it is located on low land, the slope is generally very mild and strongly affected by tidal flow. Compared to the highest tide elevation observed by PT. Barunadri Engineering Consultant at +0,213 m, it is obvious that the area is vulnerable to inundation. In addition, under such situation, the river flow will also be interferred by sea level fluctuation. Under high intensity of rainfall and maximum tide, the inundation

may get even worse as the channel is unable to deliver the flood flow properly. At the same time, the drainage system may not be effectively employed due to insufficient capacity and again enhance to more inundations within the area. Flood control management is therefore absolutely crucial to provide security from any inundations. To do so, optimizing retention pond is proposed here as an alternative solution to the flood problems.

Data Availability

Besides the daily rainfall data collected from Supadio Station for duration of 44 years (1956 – 1999), other data that also available to conduct this study includes some data obtained from the field measurement such as channel geometry and sea tide fluctuation measured at downstream of Kapuas Besar River for 73 hours (Dep. Pekerjaan Umum, 1994). While for the hydrograph information which is necessary to be included as upstream boundary, unfortunately, is not available. To estimate the required hydrograph, this study makes use of Duflow model to simulate the acquiring netto discharge of both Kapuas Kecil River (node J) and Landak River (node R). These acquiring netto discharges are then added with value of 2,000 m³/s that is estimated based on the bank full capacity of the related channels. Illustration of the whole drainage system as mentioned above is presented in the following Figure 1.

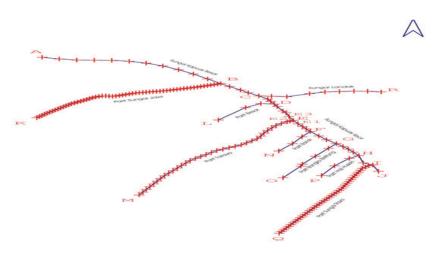


Figure 1. Channel System of Kapuas River

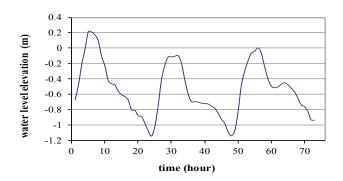
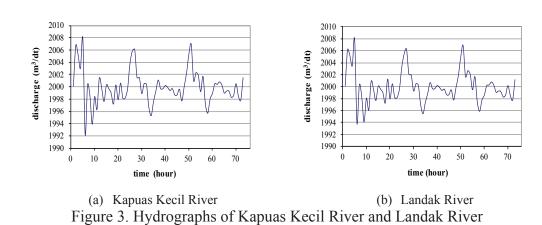


Figure 2. Sea tide fluctuation measured at Kapuas Besar River



LITERATURE STUDY

Hydrology Review

Hydrological analysis is generally a part of pre-eliminary analysis in designing waterworks. The hydrological analysis usually represents the relationship between rainfall, basin, and runoff. As it is a stochastic phenomena, asumptions taken are very critical to the next stage analysis. As regard to that, risk will always be part of hydrological analysis. Basically, waterworks have to be designed in accordance to standard designing method. By this way, it is expected the design will fit to the requirement for the setting of period. To choose the appropriate designed flood discharge with a certain period, it involves social and economic factors. It means the highest serviceability or maximum benefit with a minimum cost will basically be prioritized. According to the design standard, for the development of urban drainage, the return period that must be considered is minimum 5 years (Sri Harto, 1993).

Unsteady Flow Analysis

In analyzing the capacity of channel as regard to the influences of sea tide, the water flow analysis must be performed as unsteady flow analysis. By considering one dimensional analysis, the modeling of such hydrodynamics process can be done by help of a numerical model of Duflow (IHE Delft, 1992). Besides it provides water surface profile along the channel, it includes the ability to estimate optimum volume of retention pond. The basic equations that govern one dimensional analysis is the equation of continuity and momentum or as called as St. Venant equation.

Continuity equation :
$$\frac{\partial Q}{\partial x} + \frac{\partial A}{\partial t} = q$$
(1)

Momentum equation:
$$\frac{\partial Q}{\partial t} + \frac{\partial \left(\alpha \frac{Q^2}{A}\right)}{\partial x} + gA \frac{\partial h}{\partial x} + \frac{gQ|Q|}{C^2AR} = 0 \quad(2)$$

Using finite difference method, the above equations are then discreted into differential equations. Here, the implicit scheme of Preismann is applied to solve the problem (Cahyono, 1999). To do so, the input data required to perform the simulation are model scheme, channel geometry, initial condition, and boundary condition.

Retention Pond

In a matter a fact, the flooding management can perform either structural or non structural. Retaining facility is one of structural approach that has been widely used to control the flood flow. Referring to its function, this retaining facility can be divided into two categories: storage type and infiltration type (Doddi, 2009). Retention pond and retarding pond or regulation pond are the examples of storage type [Suripin, 2004].

The dimension of retention pond can be determined by conducting the flood routing. Many methods have been sought for predicting the characteristic features of the movement of a flood wave along a river in order to determine the actions necessary for protecting life and property from the effects of flooding and to improve the management of water related systems along natural or manmade watercourses. Flow routing may be classified as either lumped or distributed. In lumped flow routing or hydrologic routing, the flow is computed as a function

of time at one location along a watercourse. While in distributed flow routing or hydraulic routing, the flow is computed as a function of time simultaneously at several cross sections along a watercourse (Maidment, 1993).

RESULTS AND DISCUSSION

Designed Rainfall

Based on the result of frequency analysis of maximum annual daily rainfall data, the 5 years designed rainfalls obtained for various distribution probabilities are found vary from 163.908 – 176.320 mm. As shown in Table 1, it can be noticed that Gumbel probability distribution gives the best fitted value. The 5 years designed rainfall in accordance to Gumbel distribution is 170.247 mm.

Table 1. Designed rainfall under various return periods

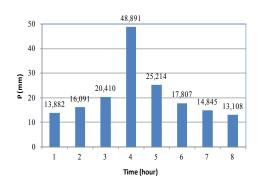
				1	
Probability Return $P(x \ge Xm)$ Period		Normal	Log Normal	Gumbel	Log Pearson III
0.9	1	70.774	84.439	79.782	87.273
0.5	2	134.482	127.385	126.316	122.630
0.2	5	176.320	166.874	170.247	163.908
0.1	10	198.189	192.172	199.334	195.248
0.05	20	216.250	215.929	227.234	228.506
0.02	50	236.576	246.200	263.349	276.731
0.01	100	250.128	268.702	290.411	317.189
0.001	1,000	288.102	343.331	379.835	483.557
Chi square v	alue	2.136	1.227	0.545	1.227
Chi critical value Smirnov value		5.991	5.991	5.991	3.841
		0.153	0.101	0.090	0.053

Rainfall Distribution

In order to estimate the rainfall distribution, this study employs Alternating Block Method (ABM) based on the available intensity duration curve (IDF). As it is derived from the short term of rainfall data, therefore, this distribution can be considered to represent the situation of local rainfall. The rainfall distribution percentage is presented in the Table 2 and Figure 4.

Table 2. Hourly	Designed	l Rainfall	for 5	Years	Return	Period
Table 2. Hours	Dosigno	a ixamman	1 101 2	1 Cars	ixciuiii .	LCIIOG

t (hour)	Δt (hour)	It (mm/ hour)	ΣIt (mm)	ΔP (mm)	%Pt	Pt
1	0-1	25.29	25.29	25.29	8.15	13.882
2	1-2	19.17	38.33	13.04	9.45	16.091
3	2-3	16.30	48.89	10.56	11.99	20.410
4	3-4	14.53	58.10	9.21	28.72	48.891
5	4-5	13.29	66.43	8.32	14.81	25.214
6	5-6	12.35	74.10	7.68	10.46	17.807
7	6-7	11.61	81.29	7.18	8.72	14.845
8	7-8	11.01	88.07	6.78	7.70	13.108
	Tota	al rainfall		88.1		170.247



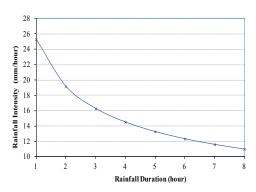


Figure 4. Hyetograph of Designed Rainfall and IDF Curve for 5 Years of Return Period

METHODOLOGY OF STUDY

This study is mainly focused on the hydraulics analysis of water surface profile and the estimation of retention pond capacity. Due to its complexity, Duflow model is therefore employed here to simulate the whole hydraulics analyses. Started from the construction of model scheme, the analyses will include the estimation of channel capacity, volume of runoff, and dimension estimation of retention pond.

RESULTS AND DISCUSSION

Based on the simulation results, it is known that there are four channels that have been experiencing flooding. Those channels are Sungai Jawi, Tokaya, Bansir and Sungai Raya. According the available master plan, the retention ponds were initially recommended to be built at Tokaya channel and Bansir channel. Due to at those both locations have insufficient space and may be densely populated in

the future, however, the location is then moved to the other two locations: Sungai Jawi channel and Sungai Raya channel. The average heights of overspill above the channel levee of Sungai Jawi channel and Sungai Raya channel are 0.211 m and 0.227 m respectively. As presented in the following Figure 5 and Figure 6, the total inundated area for both locations are 583.55 ha for Sungai Jawi channel and 151.58 ha for Sungai Raya channel.

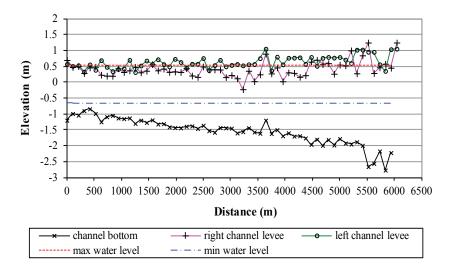


Figure 5. Water Surface Profile of Sungai Jawi Channel

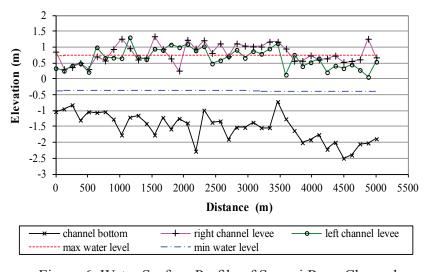


Figure 6. Water Surface Profile of Sungai Raya Channel

Retention ponds are located at upstream of the channel as it is required to have water level within flooded area can reach the retention pond and still has adequate space to cover the flooding. Based on that, it is critical to set a gate at the entrance of retention pond to control the level of inundation. Similarly for the downstream,

automatic gate is also required to avoid backwater effect coming from sea tide. By considering the level of inundation within the area, the volume of retention pond is estimated through flood routing. As regard to the inundation map which is defined by surfer software, the amount of excess runoff for Sungai Jawi drainage that must be stored at the retention is 1.750.650 m³. While for Sungai Raya Dalam, the amount of excess runoff reaches 454.740 m³. The dimensions of retention pond required for that purpose are 700 m x 700 m x 4 m and 350 m x 350 m x 4m respectively. As presented in Figure 7 below is the inundation map and sketch of required retention ponds.

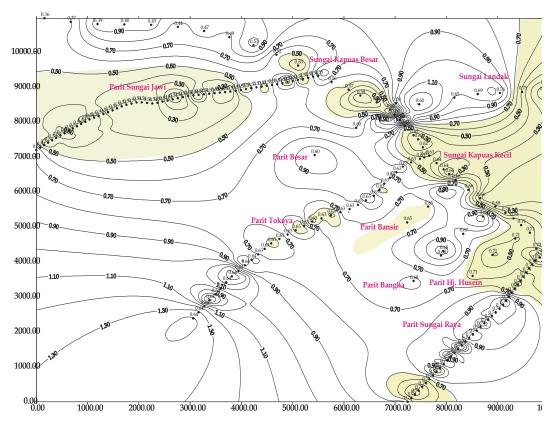


Figure 7. Inundation Map and Sketch of Required Retention Ponds

CONCLUSION AND RECOMMENDATION

The implementation of retention pond is found effective to solve the inundation problem in Southern Pontianak City. Unfortunately, the results obtained in this study cannot be further verified due to limited data available. Besides the observed river flow data, to gain better accuracy, it is necessary to have series of recorded water level information and detail topographical map.

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